

**CORTEX**

Core monitoring techniques and  
experimental validation and demonstration

# Power reactor noise theory

**CORTEX 2<sup>nd</sup> validation workshop**

Online

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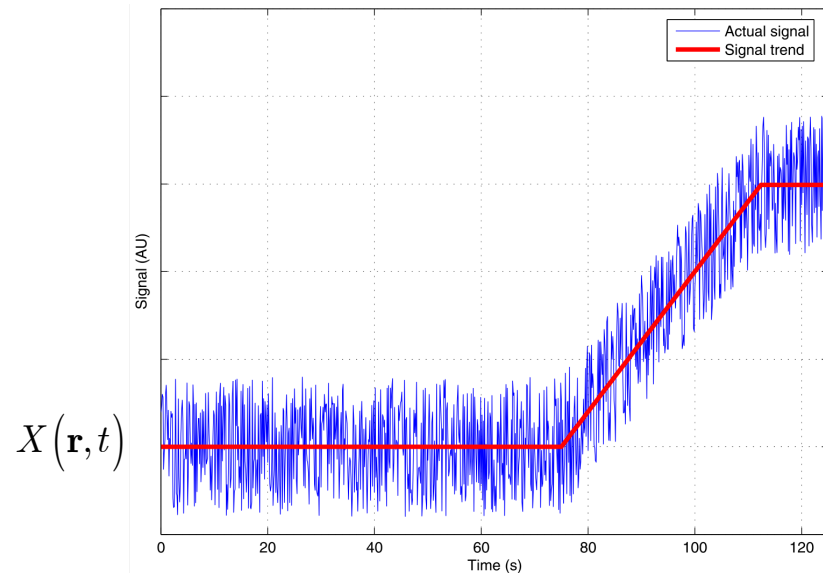
This project has received funding from the Euratom research and training programme 2014-2018 under grant agreement No 754316.

# Introduction and background



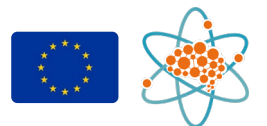
# Introduction and background

- Fluctuations always existing in dynamical systems even at steady state-conditions:



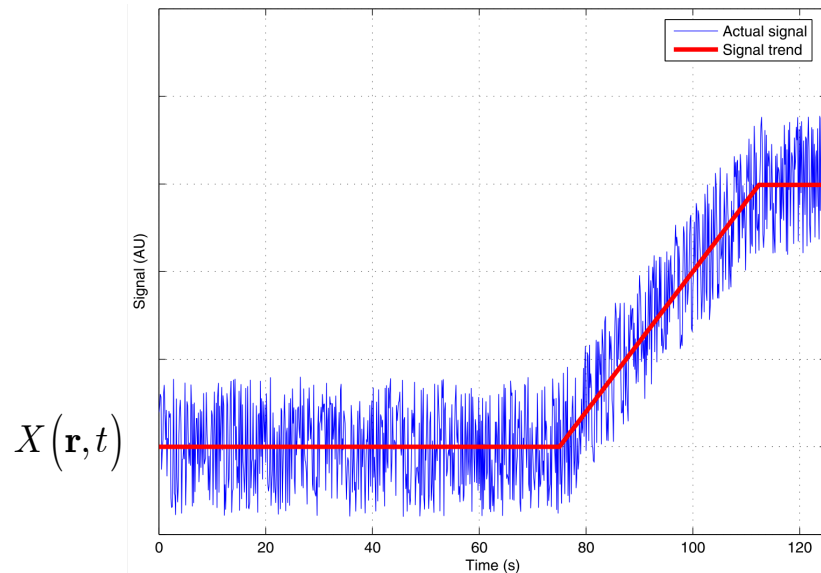
Conceptual illustration of the possible time-dependence of a measured signal from a dynamical system

$$X(\mathbf{r}, t) = X_0(\mathbf{r}, t) + \delta X(\mathbf{r}, t)$$



# Introduction and background

- Fluctuations always existing in dynamical systems even at steady state-conditions:



Conceptual illustration of the possible time-dependence of a measured signal from a dynamical system

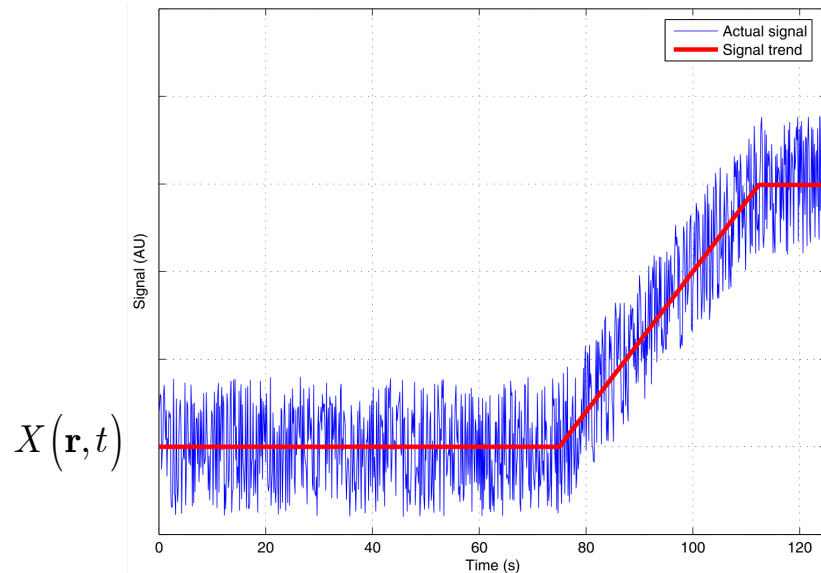
$$X(\mathbf{r}, t) = X_0(\mathbf{r}, t) + \delta X(\mathbf{r}, t)$$

actual  
signal



# Introduction and background

- Fluctuations always existing in dynamical systems even at steady state-conditions:



Conceptual illustration of the possible time-dependence of a measured signal from a dynamical system

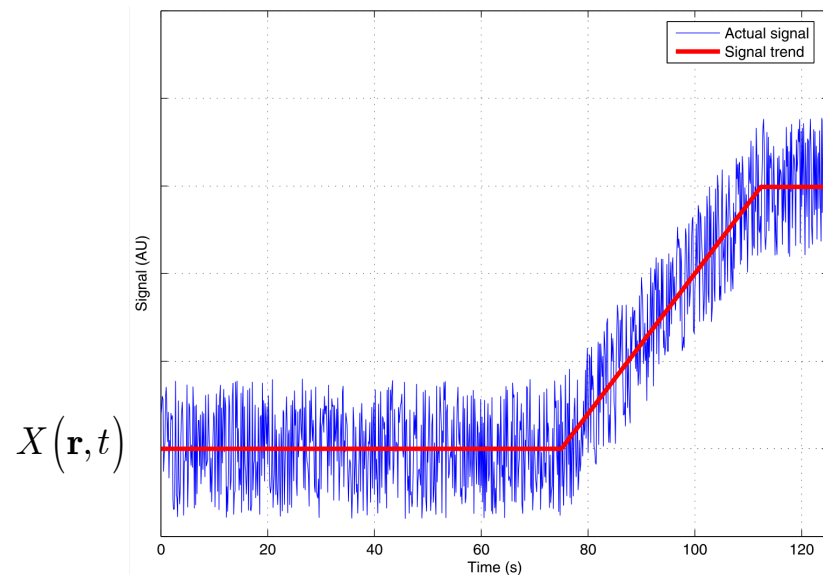
$$X(\mathbf{r}, t) = \underbrace{X_0(\mathbf{r}, t)}_{\text{signal trend or mean}} + \delta X(\mathbf{r}, t)$$

signal  
trend or mean



# Introduction and background

- Fluctuations always existing in dynamical systems even at steady state-conditions:



Conceptual illustration of the possible time-dependence of a measured signal from a dynamical system

$$X(\mathbf{r}, t) = X_0(\mathbf{r}, t) + \delta X(\mathbf{r}, t)$$

fluctuations  
or “noise”

- Fluctuations carrying some valuable information about the system dynamics



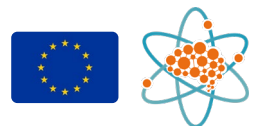
# Introduction and background

- Fluctuations could be used for “diagnostics”, i.e.:

- Early detection of anomalies
- Estimation of dynamical system characteristics

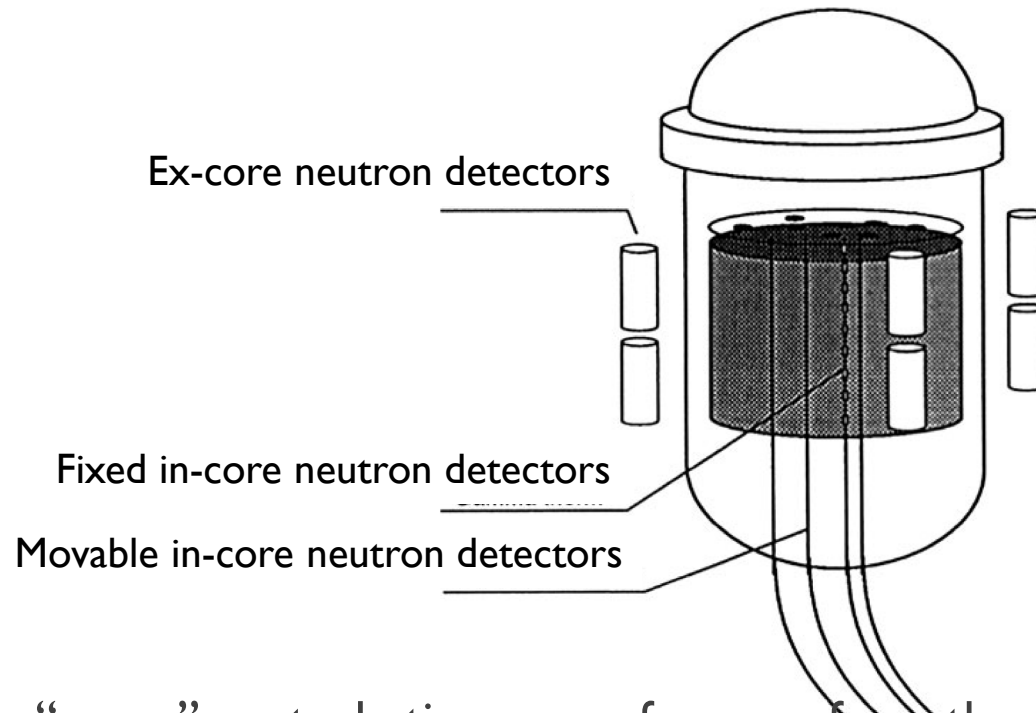
... even if the system is operating at steady-state conditions

- Fluctuations in the neutron density in nuclear reactors can be used for core diagnostics and monitoring



# Introduction and background

- Neutron detectors present both as in-core and ex-core:

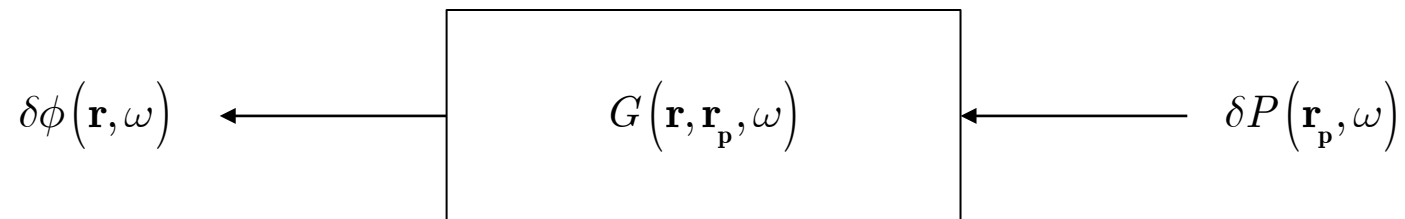


- Advantage: “sense” perturbations even far away from the perturbations
- Disadvantage: western-type reactors do not always contain many in-core neutron detectors



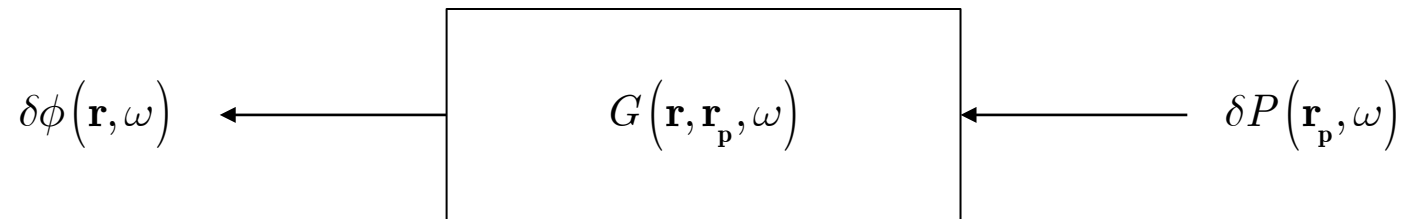
# Introduction and background

- Neutron noise diagnostics requires establishing relationships between neutron detectors and possible perturbations
- The “reactor transfer function”  $G(\mathbf{r}, \mathbf{r}_p, \omega)$  needs to be determined



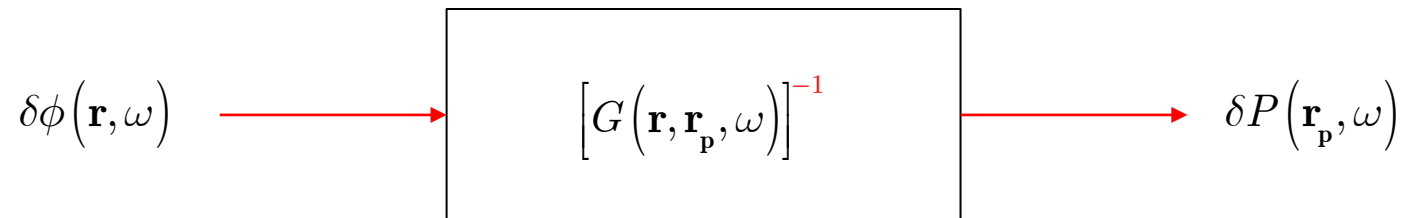
# Introduction and background

- But noise diagnostics requires the inversion of the reactor transfer function  $G(\mathbf{r}, \mathbf{r}_p, \omega)$



# Introduction and background

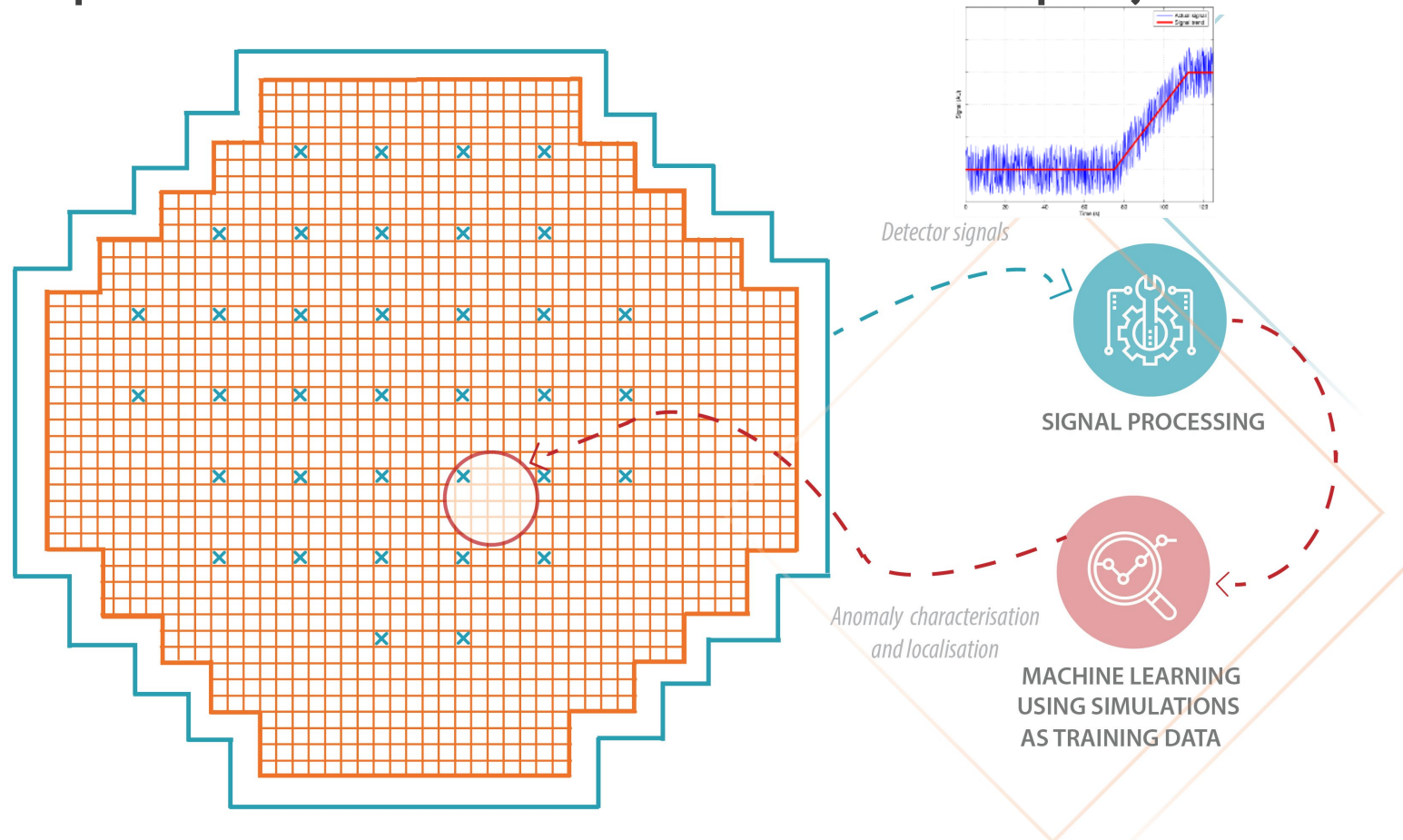
- But noise diagnostics requires the inversion of the reactor transfer function  $G(\mathbf{r}, \mathbf{r}_p, \omega)$



- Machine learning could be used for that purpose
- Unfolding possible even if very few detectors available (due to the spatial correlations existing between a localized perturbation and its effect throughout the nuclear core)

# Introduction and background

- Overall principle of the Horizon 2020 CORTEX project:

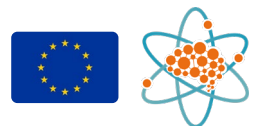


More info at:  
[cortex-h2020.eu](http://cortex-h2020.eu)



# Introduction and background

- Project aims for CORTEX:
  - WP1: Developing high fidelity tools for simulating stationary fluctuations
  - WP2: Validating those tools against experiments to be performed at research reactors
  - WP3: Developing advanced signal processing and machine learning techniques (to be combined with the simulation tools)
  - WP4: Demonstrating the proposed methods for both on-line and off-line core diagnostics and monitoring
  - WP5: Disseminating the knowledge gathered from within the project to stakeholders in the nuclear sector



# Introduction and background

- CORTEX project participants:
  - Project led and coordinated by Chalmers University of Technology
  - 18 European organizations involved in the project:
    - CEA and LGI Consulting (France)
    - Centre for Energy Research, Hungarian Academy of Sciences – MTA EK (Hungary)
    - EPFL, KKG, PSI (Switzerland)
    - GRS, ISTec, TIS, PEL, TU Dresden and TU Munich (Germany)
    - Institute of Communication & Computer Systems - National Technical University of Athens (Greece)
    - UJV (Czech Republic)
    - University of Lincoln (UK)
    - UPM and UPV (Spain)



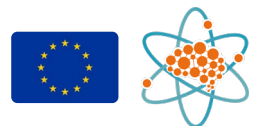
# Introduction and background

- CORTEX project participants:
  - 2 non-European organizations formally involved in the project:
    - KURRI (Japan)
    - AMS Corp (USA)
  - 7 additional organizations involved in the Advisory End-User Group:
    - IRSN (France)
    - KKG (Switzerland)
    - PEL (Germany)
    - Ringhals (Sweden)
    - Tractebel (Belgium)
    - CNAT (Spain)
    - Framatome GmbH (Germany)
    - Westinghouse Electric Sweden AB (Sweden)
    - NRG (the Netherlands)



# Introduction and background

- Modelling of the neutron noise includes two basic steps:
  - Modelling of the noise source in terms of macroscopic cross-section perturbations
  - Modelling of the neutron noise induced by fluctuations of the macroscopic cross-section perturbations
- Presentation focusing on:
  - Noise source modelling
  - Induced neutron noise modelling
  - Some theoretical remarks on power reactor noise



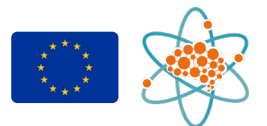


# Noise source modelling



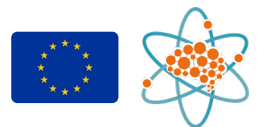
# Noise source modelling

- Perturbations can be defined:
  - In the time-domain, more or less as they are, with limitations/approximations due to the mesh used.
  - In the frequency-domain, after typically a first-order approximation of the perturbation, subsequently followed by a Fourier transform + limitations/approximations due to the mesh used.
- Modelling possibly supplemented by other modelling tools (e.g. fluid-structure modelling tool)
- Noise source modelling strongly dependent on the choices made by the user



# Noise source modelling

- Different scenarios investigated in CORTEX:
  - “Absorber of variable strength”: localized perturbation of which its amplitude varies in time at a fixed position
  - “Vibrating absorber”: lateral movement of a weak absorber
  - Axially-travelling perturbations
  - Inlet flow rate perturbations
  - Core barrel vibrations: several types of vibrations possible
  - Fuel assembly vibrations: several possible modes of vibrations



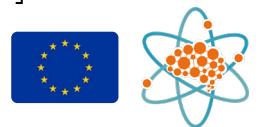
# Modelling of the induced neutron noise



# Modelling of the induced neutron noise

- Once the noise source is modelled, need to estimate the response of the neutron flux to the applied perturbation
- Could be done using the neutron transport equation (Boltzmann equation):

$$\begin{aligned} & \frac{1}{v(E)} \frac{\partial}{\partial t} \psi(\mathbf{r}, \boldsymbol{\Omega}, E, t) \\ &= -\boldsymbol{\Omega} \cdot \nabla \psi(\mathbf{r}, \boldsymbol{\Omega}, E, t) - \Sigma_t(\mathbf{r}, E, t) \psi(\mathbf{r}, \boldsymbol{\Omega}, E, t) \\ &+ \int_{(4\pi)} \int_0^\infty \Sigma_s(\mathbf{r}, \boldsymbol{\Omega}' \rightarrow \boldsymbol{\Omega}, E' \rightarrow E, t) \psi(\mathbf{r}, \boldsymbol{\Omega}', E', t) d^2\boldsymbol{\Omega}' dE' \\ &+ \frac{1}{4\pi} \int_{-\infty}^t \int_0^\infty \nu(E') \Sigma_f(\mathbf{r}, E', t') \phi(\mathbf{r}, E', t') \left[ (1 - \beta) \chi^p(E) \delta(t - t') + \sum_{i=1}^{N_d} \chi_i^d(E) \lambda_i \beta_i e^{-\lambda_i(t-t')} \right] dt' dE' \end{aligned}$$



# Modelling of the induced neutron noise

- Different approaches possible:
  - Time-domain modelling
    - Advantages:
      - Existing time-domain codes could be used
      - Non-linear effects inherently accounted for
      - Thermal-hydraulic feedback automatically taken into account
    - Disadvantages:
      - Lengthy calculations
      - Challenging to get a highly accurate solution for the noise
      - Codes originally not developed for that purpose
      - Lack of verification and validation for noise analysis

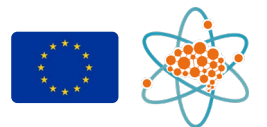


# Modelling of the induced neutron noise

- Different approaches possible:
  - Frequency-domain modelling

Time-domain equations transformed into frequency-domain equations according to the following procedure:

- Splitting between mean values and fluctuations
- Linear theory used because of the smallness of the fluctuations
- Fourier-transform of the balance equations for the dynamical part only



# Modelling of the induced neutron noise

- Different approaches possible:

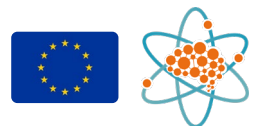
- Frequency-domain modelling

Advantages:

- Codes specifically developed for noise analysis, thus usually fully verified (validated?)
- Highly accurate noise solution
- Usually high flexibility in the modelling
- Very fast calculations

Disadvantages:

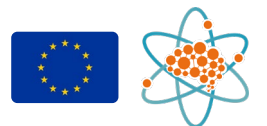
- No commercial code available
- Possible linear effects disregarded
- Thermal-hydraulic feedback generally not taken into account (but could be)





# Modelling of the induced neutron noise

- Beyond using the time- or frequency-domain, the modelling can be done in many ways:
  - Diffusion/transport
  - Deterministic/probabilistic
  - Fine/coarse spatial mesh



# Modelling of the induced neutron noise

- Codes used in CORTEX:

Code name	Domain		Non-linear terms		Angular resolution		Spatial resolution		Approach	
	Time	Frequency	Not modelled	Modelled	Diffusion	Transport	Fine-mesh	Coarse-mesh	Deterministic	Probabilistic
SIMULATE-3K	✓			✓	✓			✓	✓	
DYN3D	✓			✓		✓		✓	✓	
QUABBOX/ CUBBOX	✓			✓	✓			✓	✓	
PARCS	✓			✓	✓	(✓)		✓	✓	
FEMFUSSION	✓	✓	✓	✓	✓		✓		✓	
APOLLO3®	✓			✓		✓	✓		✓	



# Modelling of the induced neutron noise

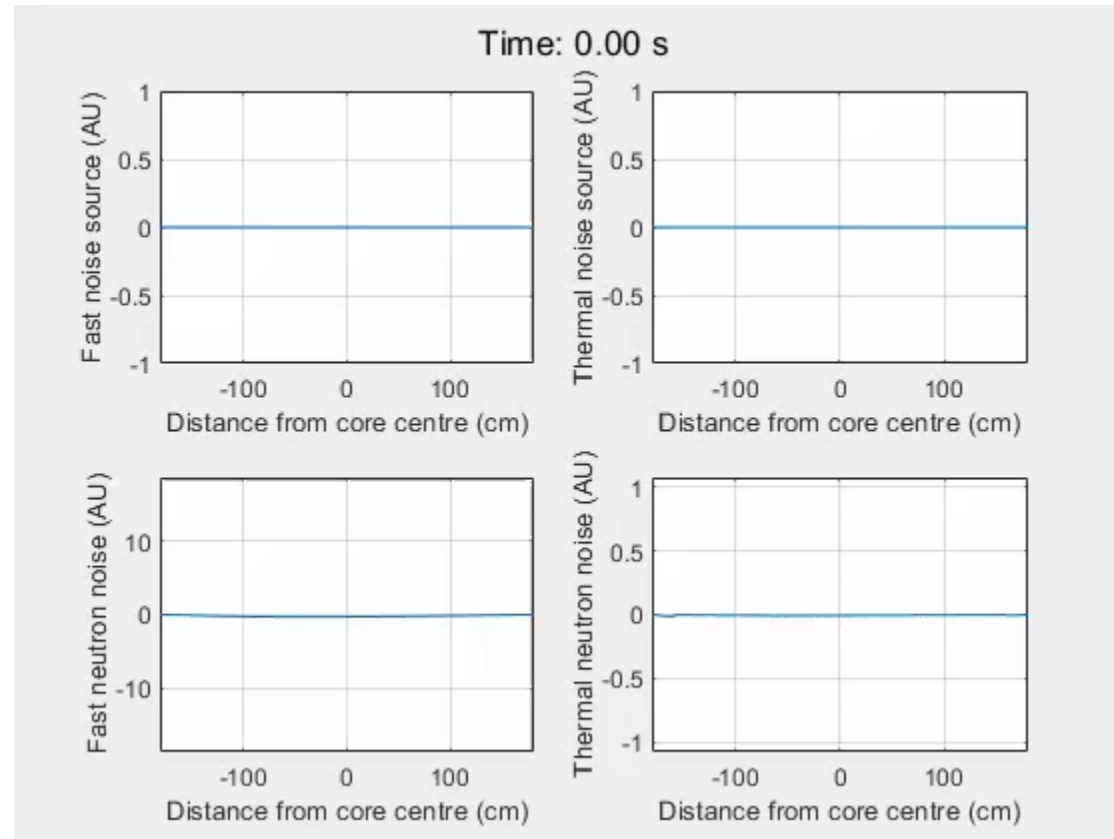
- Codes used in CORTEX:

Code name	Domain		Non-linear terms		Angular resolution		Spatial resolution		Approach	
	Time	Frequency	Not modelled	Modelled	Diffusion	Transport	Fine-mesh	Coarse-mesh	Deterministic	Probabilistic
CORE SIM		✓	✓		✓			✓	✓	
CORE SIM+		✓	✓		✓		✓		✓	
Sn-based solver		✓	✓			✓	✓		✓	
Extension of MCNP		✓	✓			✓	✓			✓
Extension of TRIPOLI-4®		✓	✓			✓	✓			✓
Equivalence-based method using MCNP		✓	✓			✓		✓		✓



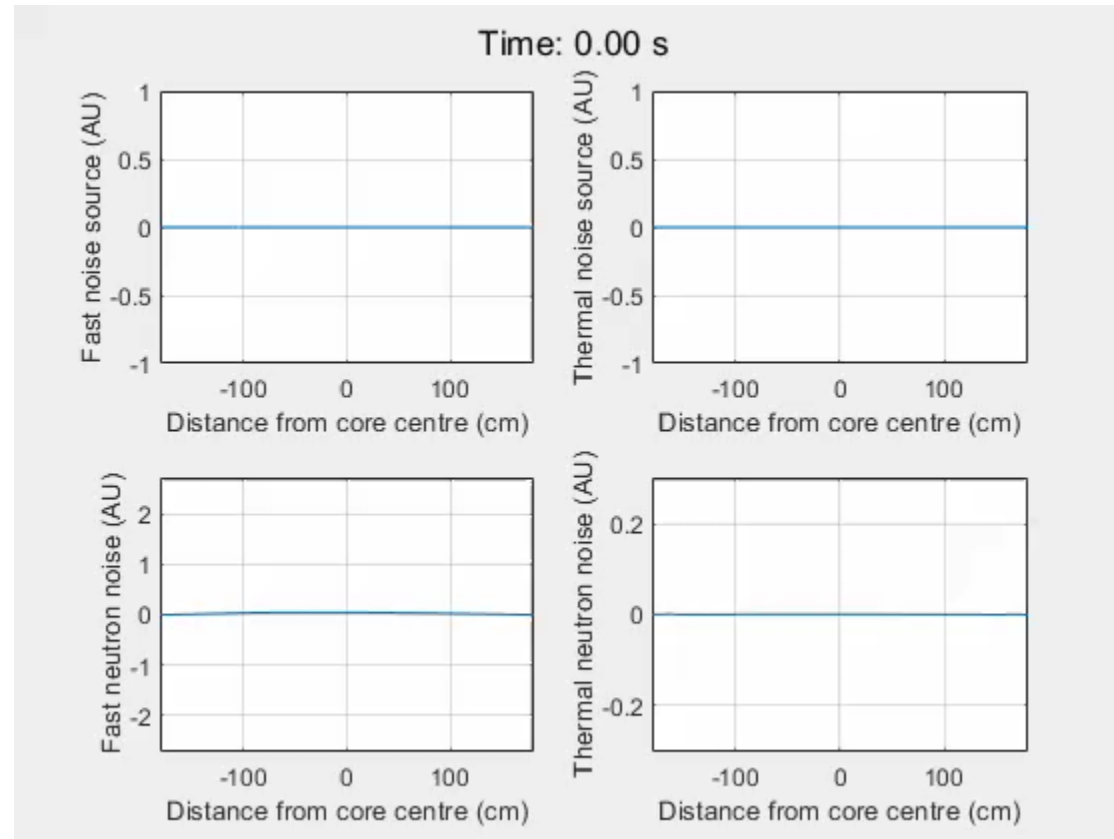
# Modelling of the induced neutron noise

- Example of an absorber of variable strength at 1 Hz in a I-D heterogeneous reactor model:



# Modelling of the induced neutron noise

- Example of a vibrating fuel assembly at 1 Hz in a 1-D heterogeneous reactor model:



# Some theoretical remarks on power reactor noise



# Some theoretical remarks on power reactor noise

- What is the point-kinetic component of the neutron noise?

Using the factorization:

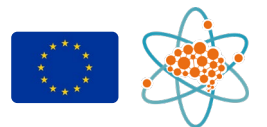
$$\phi(\mathbf{r}, t) = P(t) \cdot \psi(\mathbf{r}, t)$$

with

$P(t)$  amplitude factor  
 $\psi(\mathbf{r}, t)$  shape function

such that

$$\frac{\partial}{\partial t} \int \phi_0(\mathbf{r}) \psi(\mathbf{r}, t) d^3\mathbf{r} = 0$$



# Some theoretical remarks on power reactor noise

- What is the point-kinetic component of the neutron noise?

One obtains in first order:

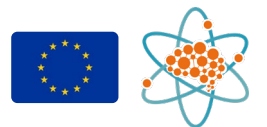
$$\delta\phi(\mathbf{r}, t) = \delta P(t) \phi_0(\mathbf{r}) + \delta\psi(\mathbf{r}, t)$$

where one assumed:

$$P_0 = 1$$

$$\psi(\mathbf{r}, t = 0) = \phi_0(\mathbf{r})$$

- Point-kinetic response:  $\delta P(t) \phi_0(\mathbf{r})$
- “Space-dependent” response:  $\delta\psi(\mathbf{r}, t)$





# Some theoretical remarks on power reactor noise

- What is the point-kinetic component of the neutron noise?

The fluctuations of the amplitude factor are further given, in the frequency domain, as:

$$\delta P(\omega) = G_0(\omega) \delta \rho(\omega)$$

with

$$G_0(\omega) = \frac{1}{i\omega \left( \Lambda_0 + \frac{\beta}{i\omega + \lambda} \right)}$$

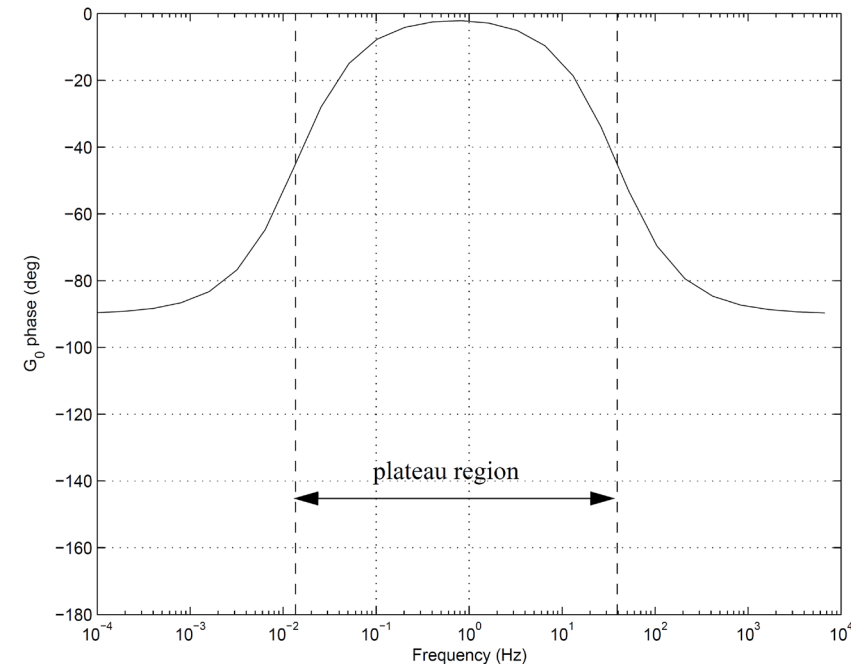
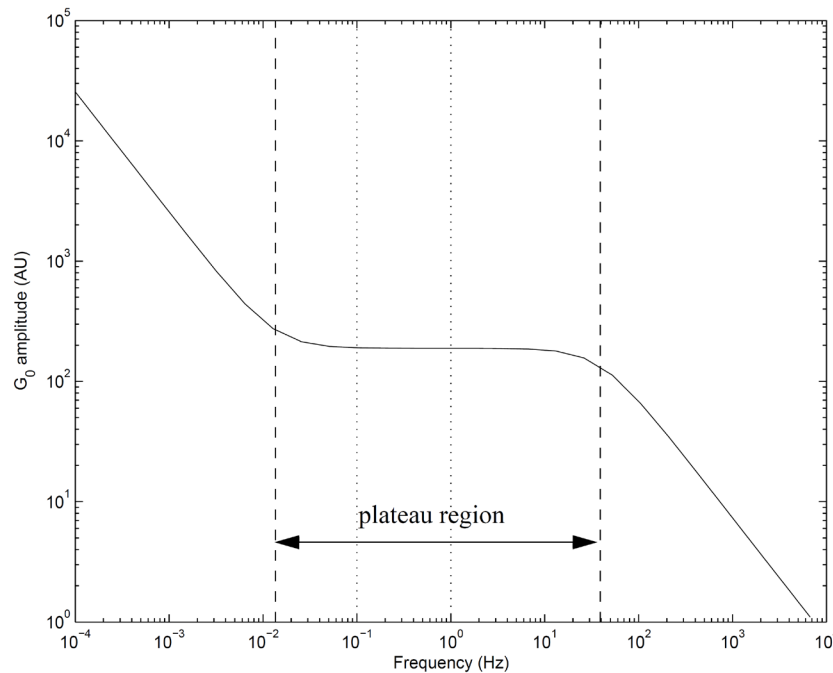
zero-power reactor transfer function

(better name: *point-kinetic* zero-power reactor transfer function)



# Some theoretical remarks on power reactor noise

- What is the point-kinetic component of the neutron noise?



Amplitude and phase of the zero-power reactor transfer function

# Some theoretical remarks on power reactor noise

- What is the point-kinetic component of the neutron noise?

Remark:

Even at zero power (i.e. without feedback), the reactor response deviates from point-kinetics in the most general case

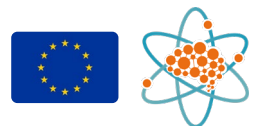


# Some theoretical remarks on power reactor noise

- What are the local and global components of the reactor noise?

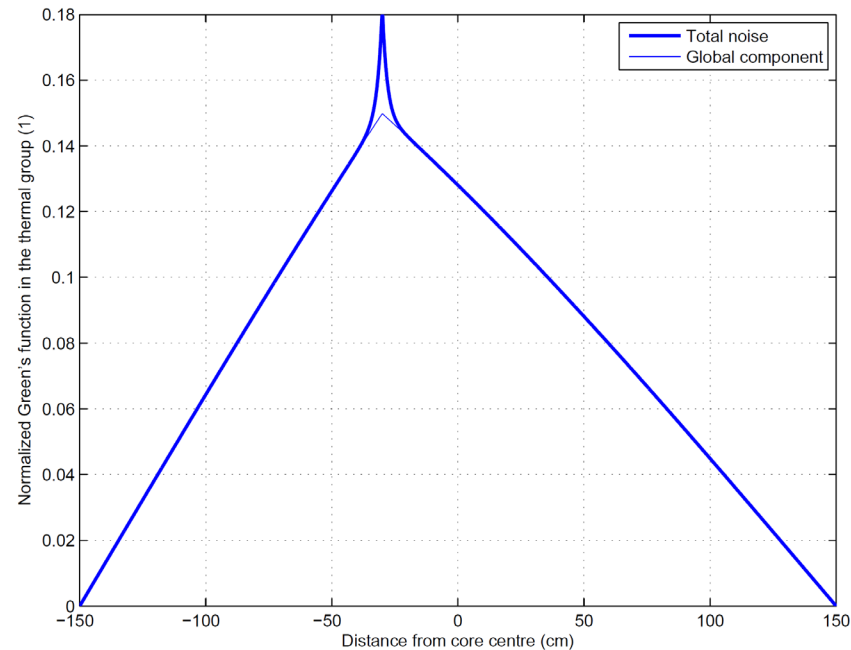
In more than or equal to two energy groups, the space-dependence of the induced neutron noise shows two relaxation lengths:

- A short relaxation length: the *local* component
- A long relaxation length: the *global* component



# Some theoretical remarks on power reactor noise

- What are the local and global components of the reactor noise?



Example of the space-dependence of the amplitude of the thermal component of the Green's function in two-group diffusion theory (at 5 Hz)

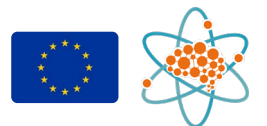


# Some theoretical remarks on power reactor noise

- What are the local and global components of the reactor noise?

Remarks:

- The local component does not exist in one-group theory!
- The global component should not be mistaken with the point-kinetic component!



# Some theoretical remarks on power reactor noise

- What are the local and global components of the reactor noise?

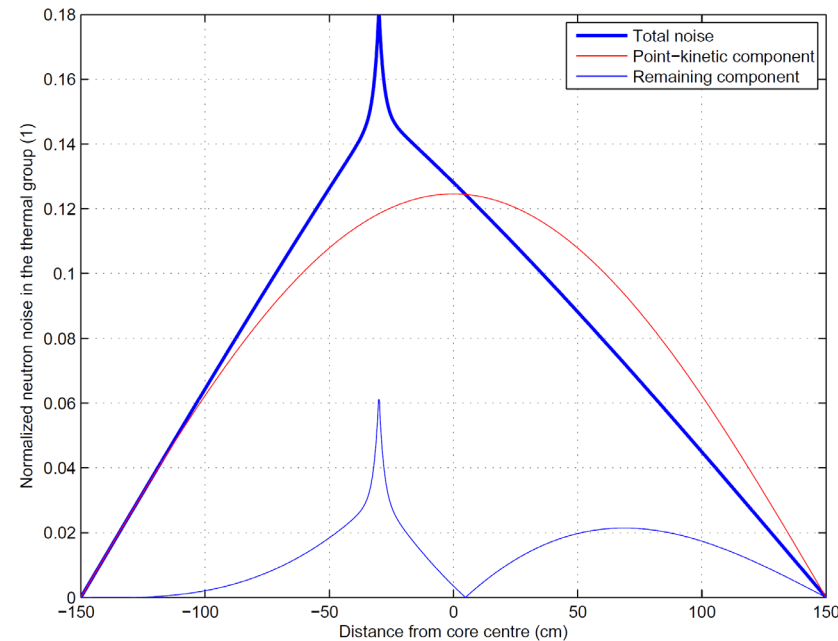
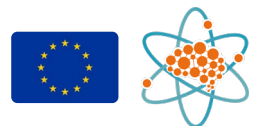


Illustration of the difference between the global component and the point-kinetic component (at 1 Hz)



# Some theoretical remarks on power reactor noise

- Go to [www.menti.com](http://www.menti.com)



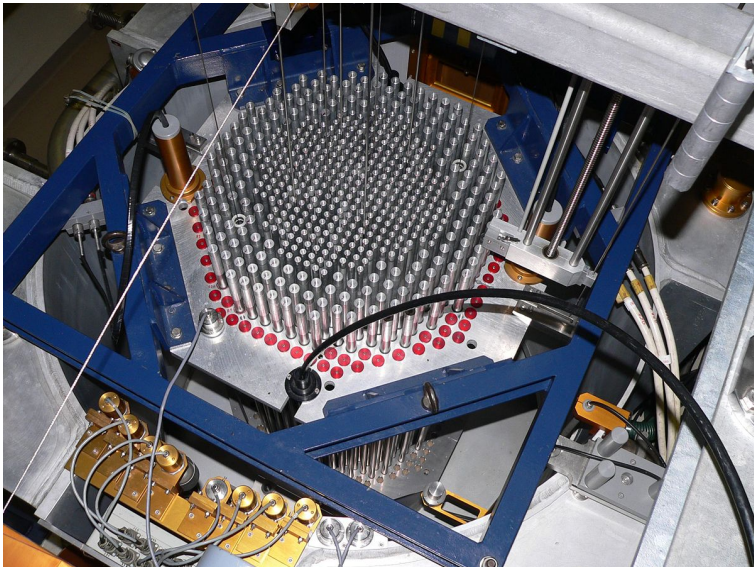


# Conclusions



# Conclusions

- Need to verify and validate the modelling tools for noise analysis
  - Purpose of this workshop:  
Illustration of the validation exercises undertaken in CORTEX using the CROCUS reactor and the AKR-2 reactor

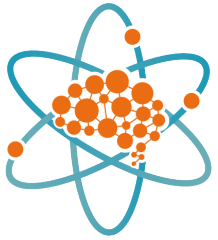


CROCUS reactor @EPFL, Switzerland



AKR-2 reactor @TU Dresden, Germany





# CORTEX

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experimental validation and demonstration

# Power reactor noise theory

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Online

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