Neutron noise experiments in the AKR-2 and CROCUS reactors for the European project CORTEX

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Abstract—The present article gives an overview of the first experimental campaigns carried out in the AKR-2 and CROCUS reactors within the framework of the Horizon 2020 European project CORTEX. CORTEX aims at developing innovative core monitoring techniques that allow detecting anomalies in nuclear reactors, e.g., excessive vibrations of core internals. The technique will be mainly based on using the fluctuations in neutron flux, i.e., noise analysis. The project will result in a deepened understanding of the physical processes involved. This will allow utilities to detect operational problems at a very early stage, and to take proper actions before such problems have any adverse effect on plant safety and reliability. The purpose of the experimental campaigns in the AKR-2 and CROCUS reactors is to produce noise-specific experimental data for the validation of the neutron noise computational models developed within this framework. The first campaigns at both facilities consisted in measurements at reference static states, and with the addition of mechanical perturbations. In the AKR-2 reactor, perturbations were induced by two devices: a rotating absorber and a vibrating absorber, both sets in experimental channels close to the core. In CROCUS, the project benefited from the COLIBRI experimental program: 18 periphery fuel rods were oscillated at a maximum of ±2 mm around their central position in the Hz range. The present article documents the experimental setups and measurements for each facility and perturbation type.

Keywords—Core monitoring and diagnostics, noise analysis, research reactor experiment, zero-power reactor

I. INTRODUCTION

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II. FIRST EXPERIMENTAL CAMPAIGN IN AKR-2

The first experimental campaign in the AKR-2 reactor took place from 6 to 15 March 2018. Two types of experiments were carried out to induce neutron flux oscillations: rotation of a thermal neutron absorber (of variable absorption with respect to the rotation angle) and linear moving of an absorber oscillating back and forth in the reactor core (a.k.a. vibrating absorber).

A. The AKR-2 reactor

The AKR-2 reactor of TU Dresden (TUD) is a thermal, homogeneous, polyethylene moderated zero-power reactor with an allowed maximum continuous thermal power of 2 W [5]. The core has cylindrical shape with a diameter of 250 mm and a critical height of 275 mm. The disk-shaped fuel elements consist of a homogeneous dispersion of polyethylene and uranium oxide – 19.8 % enriched in $^{235}$U, with an O-to-U ratio of 2.27. The $^{238}$U density in the fuel elements amounts to 0.060 g/cm$^3$. The core is surrounded by a graphite reflector with a density of 1.75 g/cm$^3$ (see Figure 1). The axial and radial thicknesses are 20 and 32 cm, respectively. Therefore, the critical mass is relatively small (about 790 g of $^{235}$U). Within certain constraints, it is a minimum-critical-mass reactor.

For safety reasons, the core consists of two separable sections. The fuel elements of each section are enclosed in a hermetically sealed aluminum container. In the shut-down position the distance between the lower and the upper core section is about 50 mm. The lower section is lifted by means of a core drive mechanism including an electromagnetic holder of the core section. Through a tube within this mechanism the start-up neutron source (Am-Be, neutron yield 2.2 $\times$ 10$^5$ n/s) is moved from the source container to the bottom side of the core. The distance between the bottom side of the core and the middle of the source container measures about 800 mm.

The reactor is controlled by three cadmium absorber plates. These plates are moved vertically in a gap within the reflector outside the reactor tank. They are designed as combined control and safety rods. An automatic reactor power control is available using the control rods. The lower core section and the control rods are held by electromagnets in their normal-operation positions. Any scram signal opens the direct-pull holding magnets allowing the rods and the lower core section to fall in the shut-down position by gravity.

The reactor core, reactor tank, graphite reflector and control rods are arranged on a horizontal steel plate (diameter 1000 mm, thickness 30 mm) inside the reactor vessel. This is a cylindrical double-walled vessel containing the biological shield and having an outer diameter of 2500 mm and a height of 2800 mm.

There are four horizontal and two vertical experimental channels with different diameters and shapes. They provide adequate in-pile irradiation volume with different neutron spectra. At 2 W power level, the maximum flux density of thermal neutrons in the central experimental channel 1-2 (see Figure 1) is about 2.5 $\times$ 10$^7$ cm$^{-2}$ s$^{-1}$.

B. Neutron detection instrumentation

The nuclear instrumentation used for the first campaign of measurements at the AKR-2 reactor is comprised by seven detection channels from which the neutron flux level in the reactor is inferred, their locations are shown in Figure 1 (right):

- Three $^3$He proportional counters (PC)
- One $^{235}$U fission chamber (FC)
- Two logarithmic wide-range monitors (WRM1 and 2), $^{235}$U fission chambers
- One linear power-range monitor (PRM3), gamma-compensated ionization chamber

![Fig. 1. The AKR-2 reactor: on the left, side cross section; on the right, cross section showing components, experimental channels (numbers), perturbation devices (green), and neutron detection instrumentation (blue and red).]
It is worth noting that the three latter channels comprise the reactor instrumentation for safety and reactor monitoring purposes. These detectors are shown in red color in Figure 1.

Three independent data acquisition systems (DAQ) were provided by TUD, EPFL and ISTec and used during the measurements for signal readout and storage. The complete neutron detection sequence with the associated electronics is available in [6].

C. Experiments

The experiments at the AKR-2 reactor consisted in introducing two different sources of periodic reactivity perturbations that induce neutron flux oscillations. The first type of perturbation is generated by a rotating neutron absorber that has a varying absorption cross-section with respect to the rotation angle, and the second one by a linearly oscillating absorber that is moved back and forth inside the reactor core (vibrating absorber). In addition to the seven neutron detection signals, three other signals were measured and recorded:

- linearly moving absorber position as a function of time,
- inductive proximity sensor’s signal to detect the rotation,
- external TTL signal for synchronization purposes.

1) Rotating absorber experiments

In order to maximize the perturbation induced to the neutron flux, the rotating absorber shaft was inserted in a location where the gradient of the neutron flux is maximum: i.e., the tangential line (channel 3-4). The reactivity worth of the absorber was measured and is presented in Appendix 7.6.1.

The geometry description and mechanical arrangement of the rotating absorber are summarized below:

- absorber material: natural cadmium (with impurities),
- dimensions of cadmium sheet (cm): 25 × 2 × 0.02,
- rotation axis location: tangential channel 3-4,
- rotation axis distance with respect to core center: 22 cm in the radial direction and 8 cm above in height,
- Cd sheet distance with respect to rotation axis: 2.98 cm.

The experimental arrangement is illustrated in Figure 2, presenting two section views of the rotating absorber with geometrical details. The static reactivity worth of the absorber was measured and is about 11 ct in total. The rotation speed was kept constant while measuring. The experiments were carried out at a frequency range from 0.2 to 2 Hz. The rotation was measured by an inductive proximity sensor, which yielded a pulsed signal per revolution.

2) Vibrating absorber experiments

A pneumatic-driven vibrating absorber was employed to linearly oscillate a neutron absorber back and forth inside the reactor core. The absorber is moved along the experimental channel 1-2, between a position inside the core and a position outside the core as illustrated in Figures 1 and 3. The static reactivity worth of the absorber was measured at 13 ct in total. The material and geometry data for the absorber are summarized below:

- linear motion axis: radial channel 1-2 at core mid-height,
- absorber thickness: 1.016 mm,
- absorber diameter: 12.7 mm,
- absorber material: 99.97% natural Cd plus impurities.

The periodic motion of the vibrating absorber is defined by two main parameters: the waiting and moving time as shown in Figure 3. The pneumatic system allows to modify the absorber motion by varying the moving time (tm) from 0.4 to 2.0 seconds, and/or the waiting time (tw) from 0.1 to 4.0 seconds. By tuning these parameters, the experiments were carried out at a frequency range from 0.08 to 0.71 Hz. The relative position of the vibrating absorber was recorded along.

![Channel 1-2](image)

![Position](image)

Fig. 3. On the top, side view of the absorber motion path in channel 1-2 (units in cm). On the bottom, trapezoidal motion followed by the absorber in the experiments.

III. FIRST EXPERIMENTAL CAMPAIGN IN CROCUS

The first experimental campaign in the CROCUS reactor took place from 17 to 21 September 2018. Vibrating fuel rods experiments were carried out using an in-core device that was specifically developed for that purpose [7], [8]. This section describes the CROCUS reactor, the experimental setup, and the vibrating fuel rods experiments.

A. The CROCUS reactor

CROCUS at the École Polytechnique Fédérale de Lausanne (EPFL) is an experimental zero-power reactor, uranium-fueled and light water-moderated, dedicated to teaching radiation and reactor physics, and to research. A complete description of the
The core is located in an Al-6060 grade vessel of 130 cm in diameter, 160 cm in height, and 1.2 cm in thickness. The vessel is filled with demineralized light water used as both moderator and reflector. The core active part has the approximate shape of a cylinder of 100 cm in height and about 60 cm in diameter. CROCUS operates at room temperature using a controlled water loop with secondary and tertiary circuits, two heat exchangers and an electrical heater.

The core can be found in the International Reactor Physics Experiments Handbook (IRPhE) [9], [10]. It has been licensed for operating at a maximum power of 100 W, i.e. a total neutron flux of $\sim 2.5 \times 10^8 \text{ cm}^{-2}\cdot\text{s}^{-1}$ at the core center. Criticality is controlled either by water level using a spillway, or by two B$_4$C absorber control rods, with an accuracy of ±0.1 mm (equivalent to approximately ±0.4 pcm) and ±0.5 mm (±0.2 pcm), respectively. CROCUS operates at room temperature using a controlled water loop with secondary and tertiary circuits, two heat exchangers and an electrical heater.

The core is located in an Al-6060 grade vessel of 130 cm in diameter, 160 cm in height, and 1.2 cm in thickness. The vessel is filled with demineralized light water used as both moderator and reflector. The core active part has the approximate shape of a cylinder of 100 cm in height and about 60 cm in diameter. It consists of two interlocked fuel zones with square lattices of different pitches: an inner zone of 336 UO$_2$ rods with an enrichment of 1.806 wt.% and a pitch of 1.837 cm; an outer zone of 176 U$_{metal}$ rods for these experiments, 0.947 wt.% and 2.917 cm; a varying water gap between the two zones because of the two different pitches. The picture of the reactor and critical assembly configuration is shown on Figure 4.

Both uranium fuels consist of a 1-m pile of cylindrical pellets cladded in aluminum. The rods are maintained vertically by two octagonal aluminum grid plates spaced 1 m apart. In the COLIBRI program, the grids have a 1 mm cadmium layer to limit axial neutron leakage to the environment, i.e. structures activation, with the active zone of the fuel starting in the middle of the lower cadmium layer.

### B. The COLIBRI experimental setup

The COLIBRI fuel rods oscillator is designed to simultaneously oscillate any of 18 metallic uranium fuel rods laterally in the west region of the core periphery zone. It consists of two moving plates set above and below the core grids, and rigidly connected by an aluminum beam (see Figure 5). Each plate carries an extremity of the fuel rods, top and bottom respectively. The top moving plate is fixed on the superior grid via gliders. Its oscillation is produced by a motor: the motor rotation is converted to a linear translation using an eccentric sheave and a rod. The oscillation is transferred to the bottom moving plate via the aluminum beam. The bottom moving plate is not constrained by gliders, it is displaced only because of its connection to the transmission beam.

The selection of the moving fuel rods is performed by letting the rods lay on the reactor base plate (non-moving), or suspend them up 10 mm above the base plate to insert them in the moving plates. Top and bottom end caps are fixed to each rod to allow the insertion in the enlarged holes of either the static grids or the moving plates. The weight of the oscillating rods is supported by a platform. The amplitude of the oscillation is precisely tuned by changing the eccentricity of the sheave with calibration plates, 0.5 mm by 0.5 mm from 0 to ±2.5 mm. Its frequency is depending on the speed of the motor.

The oscillation is controlled and monitored via a LabVIEW-developed software with 10 ms time-steps. An inductive captor is set at the rotation axis (i.e. at the top), which detects the actual movement of the motor by detecting the passage of four metallic pins per rotation. A cable coder is used to measure the displacement of the moving plate, i.e. at the bottom, with a...
0.1 mm precision. The software produces a csv file output with the recordings of the motor position and speed, the signal of the inductive captor, and the position measurement of the cable. A typical recording of an oscillation is presented in Figure 6. The inductive captor signal is also extracted for live and synchronized recording with the detection instrumentation.

The behavior of the oscillator has been characterized in air and in water, out of the vessel and in-core, empty, 1-rod and 18-rods loaded [11]. The behavior in frequency is sound. In amplitude, the device is rigid at the top, depending only on the rotation to translation conversion, and limited plays associated. At the bottom, it demonstrates inertia effects inducing an increase of the amplitude for the full 18-rods load case and above 1 Hz. This effect cannot be corrected, and thus has to be taken into account as is. The static reactivity worth of the 18 rods was measured at about 10 ct in total for a maximal amplitude of ±2.5 mm.

C. Neutron detection instrumentation

The detection instrumentation comprised the facility monitors, and different types of additional ex-core and in-core detectors, for a total of eleven detectors of various sizes and sensitivities:

- two operation monitors 195Pb-coated compensated ionization chambers (CIC): Merlin-Gerin CC54,
- two safety monitors 233U-coated fission chambers (FC): Photonis CFUM21,
- two ex-core large 235U-coated fission chambers: Photonis CFUL01,
- two in-core small BF3 proportional counters (PC): Transcommerce International MN-1,
- two in-core smaller BF3 proportional counters
- one in-core 235U-coated miniature fission chamber (MFC): Photonis CFUF34.

All detectors are based on prompt detection processes. The location of each of them with regards to the core and COLIBRI are presented in Figure 7. All four monitor detectors are set at reference positions, as presented in the CROCUS benchmark. The other detectors were set vertically at core mid-height. On the horizontal plane, the large CFUL01 fission chambers were set in the reflector at west (close to COLIBRI) and east positions. The BF3 counters were set at positions within the lattice as presented in Figure 7, in the control rod guide tube for the NW one (detector 3), and in aluminum channels for the others. The miniature fission chamber was set at core center. The general uncertainty on detector position is ±1 mm.

The operation ionization chambers and the large fission chambers were operated in current mode [2], whereas all the other detectors were operated in pulse mode using spectrometry charge preamplifiers. The detectors and their electronics were connected to the ISTec, TUD, and both EPFL pulse and current mode instrumentation, with a number of detectors depending on the number of possible inputs [6]. In addition, the safety monitors were used in MCS mode for power monitoring.

Fig. 5. The fuel rods oscillator with core structures and a few rods inserted in the device (right).

Fig. 6. Cable (blue) and inductive captor (bottom, red) signals provided by the control system (case: 1 rod in air, ±1.5 mm and 1 Hz).

Fig. 7. Top view of the COLIBRI configuration for the 1º CORTEX campaign with location of the perturbation (green), neutron detectors, and control rod.
D. Experiments

Two types of measurements were carried out: static, and a range of measurements in oscillation. The reactor was operated with the south control rod (see Figure 7), at a fixed water level of 1000 ± 0.1 mm. Following linearity tests, the power was set around 100 mW, and the water temperature was controlled at 20.0 ± 0.1 °C. In all cases, the 18 rods were lifted in the oscillation position: in the static case, the motor was off and the position was set at zero, i.e. in their nominal position within the lattice. The global reactivity effect of the oscillations was compensated to follow a stable power. In practice, the oscillation was started first, then the reactor was stabilized in power with the control rod before starting the measurement. The control rod insertion was updated along the operation and measurement.

The experiments are listed in Table I. 20 measurements were carried out in total, with limited repetition. All measurements were acquired by all four systems. The duration of each measurement was chosen to cover enough cycles of the perturbation oscillation, around 1000 except for 0.1 Hz, with a minimum time of 30 min for resolving the zero power noise. Amplitudes of limited waves at the water surface induced by oscillations were measured using the reactor instrumentation (INUS ultrasonic sensor). The oscillation is listed here in requested displacement amplitude and frequency, with a difference between requested and measured ones due to the system limitations [11]. In addition to the neutron detection signals, three other outputs were recorded:

- the synchronized signal from the inductive captor,
- the oscillator’s structured output, including motor, inductive captor, and cable,
- the two power monitors outputs.

<table>
<thead>
<tr>
<th>Amplitude (mm)</th>
<th>Measurement duration for each frequency (min)</th>
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<tbody>
<tr>
<td>±0.5</td>
<td>60</td>
</tr>
<tr>
<td>±1.0</td>
<td>60*</td>
</tr>
<tr>
<td>±1.5</td>
<td>60*</td>
</tr>
<tr>
<td>±2.0</td>
<td>60*</td>
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with repetition.

IV. CONCLUSION AND OUTLOOK

The first CORTEX experimental campaigns in the AKR-2 and CROCUS reactors were successfully carried out in 2018. The focus was on the acquisition of reference data set to qualify the acquisition systems, start the validation of the modelling tools developed within the Consortium, and orient the next campaigns. The analysis of the experiments is on-going for their help and dedication to the experiments.

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REFERENCES


TABLE I

LIST OF OSCILLATION EXPERIMENTS IN CROCUS

| Parameter Measurements in the CROCUS Reactor Using Current